III-V Diode Lasers for New Emission Wavelengths

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Two types of III-V diode lasers have been developed for new emission wavelengths. We have obtained emission at 0.9 to 1.06 μ m from quantum-well lasers with a strained InGaAs active layer and AlGaAs confining layers. Organometallic vapor phase epitaxy (OMVPE) was used to grow the layers on GaAs substrates. These InGaAs/AlGaAs lasers have achieved threshold current densities as low as 65 A/cm², differential quantum efficiencies as high as 90%, and, for devices 300 μ m wide and 1000 μ m long, continuous output powers up to 3.2 W and power efficiencies as high as 47%.

We have obtained emission at 2.27 μ m from lattice-matched doubleheterostructure lasers with a GaInAsSb active layer and AlGaAsSb confining layers grown by molecular-beam epitaxy (MBE) on GaSb substrates. These GaInAsSb/AlGaAsSb lasers have exhibited threshold current densities as low as 1.5 kA/cm², differential quantum efficiencies as high as 50%, and pulsed output powers as high as 1.8 W. These efficiencies and power values are the highest ever reported for room-temperature operation of semiconductor lasers with emission wavelengths >2 μ m. Emission from 1.8 to 4.4 μ m can potentially be achieved by changing the GaInAsSb composition.

Y EMICONDUCTOR DIODE LASERS have been highly successful because they are very efficient, compact, reliable, and suitable for economical mass production. The availability of these lasers has created many new applications in, among other areas, fiber optic communications, compact-disc players, optical memory drives, laser printers, and laser-pumped solid state lasers. The different applications generally require different emission wavelengths. For example, fiber optic communications currently require wavelengths of 1.3 or 1.55 µm because silica-based optical fibers have zero chromatic dispersion at 1.3 μ m and their lowest loss at 1.55 µm. For high-density optical memories, fast laser printers, and bar-code readers, visible emission is very advantageous because of the short wavelength. The optical pumping of lasers made from Nd:YAG (a neodymium-doped garnet comprised of yttrium, aluminum, and oxygen) is an application that requires

emission close to 0.808 μ m to match the strongest Nd⁺³ absorption band.

A diode laser basically consists of an active layer where photons are generated by carrier recombination, and confining layers with a lower refractive index and higher bandgap, which serve to confine the light and carriers. Epitaxial techniques are used to grow the layers on a single-crystal substrate. For an individual laser, the photon energy-and thus the emission wavelength-is limited to a narrow range determined mainly by the bandgap energy of the material forming the active layer. In commercial diode lasers that are used for roomtemperature applications such as those mentioned earlier, the substrate is either InP or GaAs, and the active and confining layers are III-V alloys that are lattice matched to the substrate. For the three principal types of lasers currently available, the layer and substrate materials and the range of emission wavelengths are, respectively,

- In_{1-x}Ga_xAs_yP_{1-y}/InP (by convention, the active layer is listed first and the confining layers second) on InP, 1.1 to 1.67 μm;
- Al_xGa_{1-x}As/Al_yGa_{1-y}As on GaAs, 0.7 to 0.9 μm; and
- (Al_xGa_{1-x})_{0.5}In_{0.5}P/(Al_yGa_{1-y})_{0.5}In_{0.5}P on GaAs, 0.63 to 0.67 μm.

For each type of laser, different emission wavelengths in the specified range can be obtained by changing the alloy composition of the active layer.

This article describes InGaAs/AlGaAs and GaInAsSb/ AlGaAsSb diode lasers developed at Lincoln Laboratory for emission at wavelengths not available commercially. Like commercial devices, the two new types of lasers use III-V alloys for the active and confining layers.

The InGaAs/AlGaAs lasers are similar in structure to AlGaAs/AlGaAs graded-index separate-confinementheterostructure single-quantum-well (GRIN-SCH SQW) devices [1]. In an InGaAs/AlGaAs laser, however, the lattice-matched AlGaAs active layer is replaced by an In, Ga1-x As layer that is under strain because its lattice constant is significantly greater than that of the AlGaAs confining layers. Such strained-layer InGaAs/ AlGaAs lasers are under development at many laboratories. Incorporation of In in the active layer enables the extension of the emission to wavelengths longer than those produced by AlGaAs/AlGaAs devices. By varying the x value of the $In_xGa_{1-x}As$ layer from 0.02 to 0.3, we have obtained emission at wavelengths from 0.9 to 1.06 µm. The operating characteristics of our InGaAs/Al-GaAs lasers are equal or superior to those of similar devices fabricated elsewhere, as well as to those of AlGaAs/ AlGaAs lasers. We have used InGaAs/AlGaAs lasers that emit at 0.94 or 0.97 µm to pump Yb:YAG lasers emitting at 1.03 µm [2], while InGaAs/AlGaAs lasers that emit at 0.98 µm have been used to pump Er-doped silica-fiber amplifiers operating at 1.53 μ m [3].

The GaInAsSb/AlGaAsSb lasers, which are at a much earlier stage of development than the InGaAs/AlGaAs devices, use a double heterostructure in which both the active and confining layers are lattice matched to a GaSb substrate. By using an active-layer composition of Ga_{0.84}In_{0.16}As_{0.14}Sb_{0.86}, we have obtained emission at 2.27 μ m. Emission wavelengths from 1.8 to 4.4 μ m can potentially be obtained for the range of GaInAsSb compositions that are lattice matched to GaSb. Possible

applications of GaInAsSb/AlGaAsSb lasers include optical communications that employ low-loss fluoride fibers (the theoretical loss is 0.01 dB/km at 2.55 μ m [4], compared with 0.2 dB/km for silica-based fibers), laser radars that exploit atmospheric transmission windows, remote sensing of atmospheric gases, and molecular spectroscopy.

InGaAs/AlGaAs Strained-Layer Quantum-Well Lasers

Figure 1 shows the bandgap versus lattice constant for AlGaAs and InGaAs alloys. Note that AlGaAs is almost lattice matched to GaAs over the entire composition range. InGaAs, however, cannot be lattice matched to GaAs because the lattice constant of $In_xGa_{1-x}As$ increases linearly with *x* from 0.5653 nm for GaAs to 0.6058 nm for InAs. For that range of *x*, the bandgap of $In_xGa_{1-x}As$ at room temperature decreases from 1.424 eV for GaAs to 0.35 eV for InAs according to the following equation [5]:

$$E_{o}(x) = 1.424 - 1.614x + 0.54x^{2}$$

InGaAs/AlGaAs lasers are the first successful lasers with an active layer that is not lattice matched to the substrate. The quality of lasers that incorporate latticemismatched layers has generally been poor because such layers have had a high density of dislocations. Dislocation formation can be avoided, however, by limiting the InGaAs to a sufficiently thin active layer while keeping the lattice-matched AlGaAs in thick cladding layers. In this design, the thin InGaAs layer is elastically strained (see the box, "The Concept of Strained Layers").

The first InGaAs/AlGaAs lasers were reported by



FIGURE 1. Bandgap energy versus lattice constant for AIGaAs and InGaAs.

W.T. Tsang in 1980 [6]. By incorporating as much as 4.5% In, Tsang extended the emission wavelength to 936 nm. Other reports of InGaAs/AlGaAs lasers followed [7, 8], but these devices were not very stable because the thicknesses of the active layers exceeded the critical value for dislocation formation. The first stable strained-layer laser was reported by D. Fekete et al. in 1986 [9]. Subsequently, many groups have reported InGaAs/AlGaAs strained-layer lasers with better characteristics [10–17].

In our investigation of InGaAs/AlGaAs lasers, we have varied the laser structural parameters to optimize these parameters and to understand their effects on laser properties. In evaluating laser performance, we have focused on two characteristics: threshold current density $J_{\rm th}$ and differential quantum efficiency $\eta_{\rm d}$, both of which can be derived from the measured curve of output power P versus current I. The threshold current is defined as the current at which the gain from the laser becomes equal to the cavity loss and above which the light output increases rapidly. The value of J_{th} is equal to the threshold current divided by the cross-sectional area of the laser active region. The differential quantum efficiency measures the increase in the number of photons emitted by the laser per electron-hole pair injected into the active layer. The value of η_d is obtained from the slope of the P-I curve above threshold. Lower values of $J_{\rm th}$ and higher values of $\eta_{\rm d}$ are preferable; such values reduce the current density required to attain a given laser power. We have achieved the lowest value of J_{th} and highest value of η_d thus far reported for InGaAs/AlGaAs lasers.

Structure and Epitaxial Growth

Figure 2 is a schematic diagram of the GRIN-SCH SQW laser. Laser light is generated in the thin $In_xGa_{1-x}As$ quantum-well active layer. The Al_yGa_{1-y}As GRIN confining layers, in which the *y* value increases linearly from a low value near the active layer to 0.7 away from the active layer, and the Al_{0.7}Ga_{0.3}As cladding layers together establish a waveguide to confine the optical field. To improve the interface quality and laser characteristics, we include thin GaAs layers (discussed later) that bound the InGaAs active layer. Such bounding is not used in Al_xGa_{1-x}As/Al_yGa_{1-y}As lasers.

We grew the laser structure on Si-doped n⁺-GaAs



FIGURE 2. Schematic structure of InGaAs/AIGaAs graded-index separate-confinement-heterostructure single-quantum-well (GRIN-SCH SQW) diode laser.

substrates by using organometallic vapor phase epitaxy (OMVPE) in a low-pressure vertical rotating-disk reactor [1]. In OMVPE, the pyrolysis of gaseous OMs and hydrides is used to deposit epitaxial layers (epilayers) on a heated single-crystal substrate. The deposition of $In_xGa_{1-x}As$ and $Al_yGa_{1-y}As$ proceeds by means of the following reactions:

$$x \text{In}(\text{CH}_3)_3 + (1 - x) \text{Ga}(\text{CH}_3)_3 + \text{AsH}_3$$
$$\rightarrow \text{In}_x \text{Ga}_{1-x} \text{As} + 3\text{CH}_4,$$

and

$$yAl(CH_3)_3 + (1 - y)Ga(CH_3)_3 + AsH_3$$

$$\rightarrow Al_yGa_{1-y}As + 3CH_4.$$

The flow of a small amount of H_2Se or $Zn(CH_3)_2$ dopes the layer n- or p-type, respectively. On the basis of surface morphology and photoluminescence studies on test layers, we selected growth temperatures of 800°C for the AlGaAs layers and 640°C for the InGaAs layer. The large difference between these temperatures required that growth be interrupted for periods of several minutes before (after) the InGaAs growth to cool (heat) the substrate. The lower and upper GaAs bounding layers were grown during the cooling and heating periods, respectively.

Laser Characteristics

We grew a series of laser structures with variations in

THE CONCEPT OF STRAINED LAYERS

WHEN WE GROW an epilayer on a substrate that has a different lattice constant, the misfit is accommodated either by strain or by the generation of dislocations. If the epilayer is thin enough, strain is favorable from an energy standpoint and no dislocations are generated. The high quality of the strained layer allows the fabrication of highperformance devices.

As early as 1949, F.C. Frank and J.H. van der Merwe [1] considered the accommodation of misfit across the interface between a thin epilayer and its substrate. It was not until 1976, however, that J.W. Matthews and A.E. Blakeslee [2] grew the first strained layer (GaAsP on a GaAs substrate), and only recently that researchers have investigated the device applications of the strainedlayer concept.

The critical thickness, below which a lattice-mismatched layer is strained, depends on the mechanical propercies of the epilayer material and the degree of mismatch. Figure A plots the critical thickness for In, Ga1-, As on GaAs (or Al-GaAs) as calculated by the model of Matthews and Blakeslee [3]. As xincreases, the mismatch increases, and the critical thickness rapidly decreases. The thickness of the active laver in a diode laser is limited to the critical thickness because the dislocations present in thicker layers will significantly degrade both the optical and electrical



FIGURE A. Critical layer thickness of $In_xGa_{1-x}As$ layers on GaAs substrates as a function of *x*. (Note: Because AIGaAs has almost the same lattice constant as GaAs, the figure also applies to $In_xGa_{1-x}As$ layers on thick AIGaAs layers.)

characteristics.

Figure B schematically compares the two cases in which the epilayer thickness is respectively below and above the critical thickness. In a strained layer (Figure B[1]), the lattice constant in the direction parallel to the interface approximately matches that of the substrate. For InGaAs on GaAs, the epilayer is under in-plane biaxial compression. In the direction normal to the interface, the epilayer is elongated so that the lattice becomes tetragonal



FIGURE B. Schematic diagram showing the lattice of (1) a strained layer, which is thinner than the critical thickness, and (2) a relaxed layer, which is thicker than the critical thickness.

rather than cubic. When the critical thickness is exceeded, misfit dislocations are generated at the growth interface and propagate back to the substrate-epilayer interface (Figure B[2]). Some of the dislocations are terminated by the formation of edge dislocations, but a considerable fraction of the dislocations propagates to the upper layer by threading. For a sufficiently thick layer, the lattice constant becomes equal to the bulk lattice constant, and the lattice is said to be fully relaxed.

The strain alters the structure of the energy bands, especially that of the valence bands. For a III-V semiconductor with a zinc-blende structure, Figure C compares the uppermost valence bands without strain and the same bands under biaxial compression. For the unstrained case, the heavy- and lighthole bands are degenerate at the Brillouin zone center. (The terms

heavy and light denote a hole's effective mass, which is inversely proportional to $d^2 E/dk^2$, where E denotes energy and k momentum. Note that $d^2 E/dk^2$ is the curvature of the energy band.) The biaxial compression changes the band structure in three ways. First, the bandgap energy is increased. Second, the degeneracy at the Brillouin zone center is removed, and the separation between the heavy- and light-hole bands increases with strain. Finally, the valence bands become anisotropic. In the direction normal to the plane of the surface, the highest band has a heavy effective mass. In the parallel direction, however, the highest band has a light effective mass.

The change in the band structure of the strained layer has a significant implication for laser performance. In order to reach population inversion, the quasi-Fermi level must be separated by more than the bandgap energy. The number of carriers required to reach this condition is smaller for a smaller density of states. In quantumwell structures, the density of states is proportional to the effective mass in the parallel direction. Thus, because the effective mass in the parallel direction for compressively strained InGaAs is smaller than that for GaAs, we expect InGaAs/Al-GaAs lasers to have lower threshold current densities than GaAs/AlGaAs lasers of a similar structure.

References

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FIGURE C. Band structure of InGaAs near Brillouin zone center for the case of (1) no strain and (2) biaxial compression.

Table 1. Effect of GaAs Bounding-Layer Thickness <i>t</i> on the Characteristics of In _{0.25} Ga _{0.75} As/AlGaAs Diode Lasers					
Wafer	<i>t</i> (nm)	$J_{\rm th}$ (A/cm ²)	λ(nm)		$\eta_{\sf d}$ (%)
А	× <u>—</u>	550	970		46
В	5	150	1024		74
С	10	125	1022		80
D	15	130	1025		80

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bounding-layer thickness *t* and InAs mole fraction *x*. Broad-stripe lasers either 100 or 300 μ m wide were fabricated by the following procedure. A photolithographic lift-off process defined stripes of Ti/Au on the p⁺-GaAs surface of a wafer. To reduce current spreading, we etched the p⁺-GaAs layer and a part of the p-AlGaAs cladding layer from the areas between the stripes by immersing the wafer in a H₂SO₄:H₂O₂:H₂O solution. The wafer was then lapped to a thickness of ~100 μ m, and the n-GaAs surface was metallized with Ge/Au/Ni/Ti/ Au at 380°C in a H₂ atmosphere. Next, the wafer was cleaved into individual bars with cavity length *L* ranging from 300 to 1500 μ m. Using a calibrated 1-cm-diameter Si photodiode detector, we measured the P-I curve of each laser in pulsed operation.

Effect of bounding layers. Lasers with $L = 500 \,\mu\text{m}$ were fabricated from four wafers. Wafer A had no bounding layers (t = 0), while wafers B, C, and D had bounding layers with t = 5, 10, and 15 nm, respectively. Except for this variation in t, the wafers were identical, with x = 0.25, $\gamma = 0.2$ to 0.7, and active-layer thickness d = 7 nm. The surface morphology was rough for wafer A, showed slight texture for wafer B, and was very smooth for wafers C and D. Table 1 summarizes the operating characteristics of the lasers. Note that lasers with t = 10and 15 nm had almost the same characteristics: $J_{th} = 125$ and 130 A/cm², respectively, and $\eta_d = 80\%$. The performance of lasers with t = 5 nm was slightly degraded, with $J_{\rm th} = 150$ A/cm² and $\eta_{\rm d} = 74\%$. For the lasers without bounding layers, $J_{\rm th}$ rose sharply to 550 A/cm² and $\eta_{\rm d}$ fell to only 46%. In addition, the emission wavelengths shifted from ~1020 nm for lasers with bounding layers to ~970 nm for those without, as a result of the increase in $J_{\rm th}$ and the associated increase in

the filling of the energy bands.

By characterizing additional laser structures with asymmetric bounding layers, we found that the upper bounding layer was essential, while the lower bounding layer had only a very small effect. Auger electron spectroscopy and photoluminescence measurements on test wafers revealed that the upper bounding layer was effective in suppressing the diffusion of In out from the InGaAs layer during the heating period when the substrate temperature was raised from 640 to 800°C.

The optimum thickness of the bounding layer depends on the InAs mole fraction in the active layer. As will be discussed later, for lasers with smaller *x*, thinner bounding layers are preferable because carrier leakage from the active layer to the bounding layers decreases with decreasing *t*. For smaller values of *x*, thinner bounding layers are sufficient to suppress In out-diffusion.



FIGURE 3. Laser emission wavelength as a function of x in the $ln_xGa_{1-x}As$ active layer for a cavity length $L = 500 \ \mu m$.

Effect of InAs mole fraction. Broad-stripe lasers were fabricated from wafers with x ranging from 0 to 0.3. To increase the optical confinement and hence reduce J_{th} , the value of y in the confining layers was graded from 0.08 to 0.7, except for three wafers in which x = 0, 0.02, and 0.05. For these three wafers, y was graded between 0.2 and 0.7, and t was varied from 0 to 1.5 nm. For one wafer with x = 0.05, t was 5 nm, and for all the other wafers, t was 10 nm.

We found that the laser characteristic most affected by a change in x was the emission wavelength. Figure 3 plots the emission wavelength versus x for $L = 500 \ \mu m$. As x increases from 0 to 0.3, the emission wavelength increases from 850 to 1060 nm. The measured wavelengths are in good agreement with theoretical values (the solid line in Figure 3) calculated [5] by taking into account three factors: (1) the bulk bandgap energy of InGaAs alloys, (2) the increase in bandgap energy due to compressive strain, and (3) the increase



FIGURE 4. Threshold current density J_{th} as a function of x in the active layer.

in the electron-hole transition energy due to the quantization of the energy levels in the quantum well. Because of the limitation imposed by the critical thickness discussed earlier, the longest wavelength that InGaAs/AlGaAs lasers can attain is ~1100 nm. Lasers with layers in which y was graded from 0.2 to 0.7 (denoted as 0.2–0.7 GRIN) had somewhat shorter emission wavelengths than the theoretical values because the quantized level was higher than expected. For x = 0.05, the emission wavelength was 882 nm with

0.2–0.7 GRIN layers, compared to 895 nm with 0.08–0.7 GRIN layers.

Figure 4 shows the dependence of J_{th} on x. For devices with t = 10 nm and 0.08–0.7 GRIN layers, the value of J_{th} is nearly constant at 110 to 120 A/cm² for $0.15 \le x \le 0.25$. These values are much smaller than the 200 A/cm² obtained for GaAs/AlGaAs lasers with 0.2–0.7 GRIN layers. The reduction in J_{th} in InGaAs/AlGaAs lasers had been predicted [18, 19] because the compressive strain reduces the density of states—i.e., the number of allowed electronic states per unit energy—in the valence band of InGaAs (see the box, "The Concept of Strained Layers"). The effect of the difference in the GRIN layers is minor: for x = 0.25 the change from 0.08–0.7 to 0.2–0.7 GRIN layers increases J_{th} from 114 to only 125 A/cm².

For $x \le 0.1$ and t = 10 nm, the value of J_{th} increases because the strain is reduced and the shallower well depth increases the leakage current from the quantum well to the bounding layers. For x = 0.05, the value of J_{th} is equal to 263 A/cm². We reduced the leakage current by decreasing t and increasing the minimum value of y. By decreasing t to 5 nm, we reduced the value of J_{th} to 216 A/cm². The value of J_{th} was further reduced to 186 A/cm² by a decrease in t to 1.5 nm coupled with the use of 0.2–0.7 GRIN layers.

For x = 0.3 and t = 10 nm, the value of J_{th} is 140 A/cm², a slight increase from the J_{th} values for the range $0.15 \le x \le 0.25$. The increase might result from an unoptimized value of t or some nonradiative recombination mechanism that increases with x.

Figure 5 shows the dependence of η_d on *x*. The value



FIGURE 5. Differential quantum efficiency η_d as a function of *x* for lasers with $L = 500 \ \mu$ m.



FIGURE 6. Dependence of threshold current density J_{th} on reciprocal cavity length 1/L for In_{0.25}Ga_{0.75}As/AlGaAs diode lasers.

of η_d is between 80 and 85% for x > 0.15. For x < 0.1and t = 10 nm, the value of η_d decreases to between 72 and 76% because of the increase in leakage current to the bounding layers. Reducing the leakage current increases the value of η_d . For lasers with x = 0.05, t = 1.5nm, and 0.2–0.7 GRIN layers, the value of η_d is 83%.

Effect of cavity length. We measured the P-I characteristics of lasers with x = 0.25 for L values ranging from 300 to 1500 μ m. Figure 6 shows J_{th} as a function of 1/L. As L increases, the value of J_{th} decreases monotonically because the output coupling loss normalized to L decreases. For $L = 1500 \ \mu m (1/L = 6.7 \ cm^{-1})$, the value of J_{th} is equal to 65 A/cm²—the lowest value obtained for any InGaAs/AlGaAs laser.

Figure 7 is a plot of η_d^{-1} versus *L*. The value of η_d for $L = 300 \ \mu m$ is 90%—the highest value obtained for InGaAs/AlGaAs lasers. Because of photon loss inside the cavity, the value of η_d decreases monotonically as L is increased. From Figure 7, we can deduce the internal quantum efficiency η_i and the internal loss coefficient α_i for photons. The parameter η_i is defined as the number of emitted photons per injected electron above threshold. The value depends on the efficiency of carrier collection to the active layer and the ratio of radiative to nonradiative recombination. The parameter α_i measures how strongly photons are absorbed or scattered as they propagate along the waveguide. In most lasers, the loss is dominated by free-carrier absorption. A smaller value of $\alpha_{\rm i}$ is desirable because the value of $\eta_{\rm d}$ is less sensitive to L for small α_i . Since the thermal resistance is inversely proportional to L, a higher output power is expected

from lasers with a lower value of α_i . The relationship between η_d , η_i , and α_i above threshold is

$$\eta_{\rm d}^{-1} = \eta_{\rm i}^{-1} \left[\frac{\alpha_{\rm i} L}{\ln(1/R)} + 1 \right]$$

where *R* is the facet reflectivity. From Figure 7, the value of η_i is approximately 100% (obtained from the *y*-intercept) and the value of α_i is approximately 5 cm⁻¹ (obtained from the slope). By reducing the carrier density near the active region, we have obtained values of α_i as small as 1.5 cm⁻¹ in other laser structures.

From Figure 6, we can deduce the gain coefficient β , which measures the rate with which the optical gain increases as the current is increased, and the transparency current density J_{tr} , which is the value at which the active layer neither absorbs nor amplifies the light at the lasing wavelength. Both of these quantities are related to the density of states. Because the density of states is smaller for compressively strained InGaAs than for GaAs, a lower value of J_{tr} and a higher value of β are expected. The relationship between J_{th} , J_{tr} , and β is given by

$$J_{\rm th} = \frac{1}{\eta_{\rm i}} \left[J_{\rm tr} + \frac{d}{\beta \Gamma} \left(\alpha_{\rm i} + \frac{\ln\left(1/R\right)}{L} \right) \right], \qquad (1)$$

where Γ is the confinement factor, which is defined as the fraction of light in the active layer. From the slope of the curve in Figure 6, we calculate the value of β to be 0.085 cm μ m A⁻¹, about 60% higher than the value obtained for GaAs/AlGaAs quantum-well lasers. Using Equation 1 along with the *y*-intercept and the values $\alpha_i = 5 \text{ cm}^{-1}$ and $\Gamma = 0.025$, we obtain $J_{\text{tr}} = 25 \text{ A/cm}^2$ —



FIGURE 7. Dependence of reciprocal differential quantum efficiency η_d^{-1} on cavity length *L* for In_{0.25}Ga_{0.75}As/AIGaAs diode lasers.



FIGURE 8. Dependence of threshold current density J_{th} on temperature for In_{0.25}Ga_{0.75}As/AIGaAs diode laser 300 μ m wide \times 1500 μ m long.

the lowest value reported for any semiconductor laser.

Effect of temperature on J_{th} . The value of J_{th} increases with temperature because of a decrease in gain and an increase in leakage current as well as the effects of nonradiative recombination. Figure 8 shows the temperature dependence of $J_{\rm th}$ for 1500-µm-long devices with x = 0.25. The value of J_{th} increases from 65 A/cm² at 25°C to 90 A/cm² at 75°C. The temperature dependence of J_{th} is typically described by the characteristic temperature T_0 that appears in the expression $J_{th}(T) =$ $J_0[\exp(T/T_0)]$, where T is the absolute temperature and J_0 is an empirical parameter. Higher values of T_0 are preferable because they imply that J_{th} is less sensitive to temperature. The value of T_0 for the device shown in Figure 8 is 178 K between 25° and 45°C and 141 K between 55° and 75°C. The value of T_0 in the lower temperature range decreases with decreasing cavity length to 159 K for $L = 1000 \ \mu m$, and 137 K for L =300 μ m. These values are comparable to those obtained for GaAs/AlGaAs quantum-well lasers.

Continuous-Wave Operation

For continuous-wave (CW) operation, several devices with x = 0.25 were mounted junction side down on copper heat sinks with In solder. A thermopile detector measured the output power. Figure 9 shows the P-I curve for an uncoated laser with $L = 1000 \,\mu\text{m}$ and width $W = 300 \,\mu\text{m}$. The threshold current is about 240 mA, and η_d is about 62%. The maximum output power from both facets is limited to 3.2 W by the junctiontemperature rise. Figure 9 also shows the power conversion efficiency, the total optical power divided by the electrical power input. The power efficiency is always smaller than η_d because of the finite values for threshold current and series resistance. With a series resistance of about 0.07 Ω , the maximum power efficiency is about 47%. The power efficiency decreases at higher currents because the junction-temperature rise reduces η_d .

Reliability

In view of the high strain levels in the active layer, the reliability of InGaAs/AlGaAs lasers has often been questioned. Several experiments, however, indicate that these lasers will prove to exhibit greater reliability than the more mature GaAs/AlGaAs lasers [11, 20, 21]. A dramatic demonstration of the comparative reliability of InGaAs/AlGaAs and GaAs/AlGaAs lasers has been reported by R.G. Waters et al. [21]. To accelerate degradation, damage was introduced by scribing a line next to the active stripe. The GaAs/AlGaAs lasers degraded rapidly by the propagation of dark-line defects, the dislocation networks that are the most common cause of sudden degradation in such lasers. On the other hand, InGaAs/AlGaAs lasers showed stable operation because the formation of dark-line defects was greatly reduced. The most plausible explanation for the greater reliability of InGaAs/AlGaAs lasers is lattice hardening that results because In atoms are significantly larger than



FIGURE 9. CW output power and power conversion efficiency versus current for an InGaAs/AlGaAs laser $300 \ \mu m$ wide $\times 1000 \ \mu m$ long.

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FIGURE 10. Schematic diagram of the structure of a ridge-waveguide laser.

 5×10^{-3} .

Ga, Al, and As atoms, all of which are nearly the same size [22]. However, InGaAs/AlGaAs lasers with an active layer thicker than the critical thickness degrade very rapidly because dislocations are formed to accommodate the lattice mismatch with the confining layers.

Narrow-Stripe Lasers

For many applications, lasers with low threshold currents are desirable. Confining both the current and optical field of a laser reduces the threshold current. For a tight optical mode, the waveguide must have a sufficiently large refractive-index step Δn in the direction parallel to the epilayer. If Δn is too large, however, multiple modes can be supported, and the optical field can switch to a higher-order mode as the power is increased. For the mode to be stable over a wide power range, the waveguide should support only a single mode. The



FIGURE 11. Output power versus current for InGaAs/ AIGaAs ridge-waveguide laser.

ver, mulfield can process etches GaAs and AlGaAs at the same rate, and it produces very little undercutting beneath the photore-

sist. The insulating silicon-nitride layer, which covers the entire surface except the mesa center, confines the current. A Ti/Pt/Au metallization was used to make ohmic contacts to the p⁺-GaAs layer.

optimum Δn increases with decreasing stripe width. For

3- μ m-wide stripes, the optimum Δn is approximately

We selected a ridge-waveguide structure (Figure 10)

for index-guided lasers because this structure is relatively simple to fabricate. In ridge waveguides, the value of Δn

is determined by the difference in the thicknesses of the

p-AlGaAs cladding layer in the etched and unetched

regions. The depth of etching is thus crucial for obtain-

plasma formed by a mixture of BCl3 and Ar gases. This

To etch the ridge, we used reactive ion etching in a

ing the appropriate Δn for a single-mode waveguide.

Figure 11 shows the P-I characteristic of a pulsed ridge-waveguide laser with x = 0.15 and uncoated facets. The threshold current is about 8 mA and η_d is 80%. The maximum power from both facets is more than 400 mW. The far-field pattern parallel to the junction is shown in Figure 12 at six current levels in 50-mA steps. The figure shows a fundamental Gaussian mode with a full width at half maximum (FWHM) of ~23° up to 200 mA. At 250 mA, the far-field pattern becomes slightly asymmetric, indicating that the first-order mode has begun to lase. At 300 mA, the asymmetry is more apparent.

We have operated ridge-waveguide lasers with un-



FIGURE 12. Far-field pattern of InGaAs/AlGaAs ridgewaveguide laser at six different current levels in 50-mA steps, from 50 mA to 300 mA.

coated facets in CW mode up to a level of 30 mW per facet. The output power was limited by the temperature rise that resulted from heating due to the series resistance.

GaInAsSb/AlGaAsSb Double-Heterostructure Lasers

Figure 13 shows the bandgap energy versus lattice constant for GaInAsSb and AlGaAsSb alloys at room tem-



FIGURE 13. Bandgap energy versus lattice constant for GalnAsSb and AlGaAsSb at 300 K.

perature. Lines that connect the binary compounds represent ternary alloys, and the shaded regions bounded by the lines represent quaternary alloys. The compositions of $Ga_{1-x}In_xAs_ySb_{1-y}$ alloys that are lattice matched to GaSb satisfy the following relationship:

$$y = \frac{0.91(1-x)}{1+0.05x}.$$

In Figure 14, the room-temperature values of the bandgap energy $E_{\rm g}$ and corresponding wavelength $\lambda_{\rm g}$ of the lattice-matched alloys are plotted versus *x*. Note that $E_{\rm g}$ is almost constant for x < 0.4 and has a minimum of 0.28 eV ($\lambda_{\rm g} = 4.4 \,\mu{\rm m}$) at x = 0.22.

We chose AlGaAsSb for the laser cladding layers because, unlike GaSb, it has a lower refractive index than GaInAsSb and provides potential barriers high enough to confine both electrons and holes to the GaIn-



FIGURE 14. Bandgap emission wavelength and energy at 300 K versus *x* for $Ga_x In_{1-x} As_y Sb_{1-y}$ lattice matched to GaSb, with y = 0.91(1 - x)/(1 + 0.05x).

AsSb layer. Since AlSb and GaSb have a lattice mismatch of $\sim 6.5 \times 10^{-3}$ (about five times larger than that between AlAs and GaAs), a small amount of As needs to be incorporated to avoid misfit dislocations.

The first GaInAsSb/AlGaAsSb diode lasers were reported by N. Kobayashi et al. [23] in 1980. These devices, which used a Ga_{0.95}In_{0.05}As_{0.04}Sb_{0.96} active layer and Al_{0.2}Ga_{0.8}As_{0.02}Sb_{0.98} cladding layers, operated at room temperature with an emission wavelength of 1.8 μ m and J_{th} as low as 5 kA/cm². Since then, improving the quality of the epilayers and increasing the Al content of the cladding layers have gradually reduced the value of J_{th} [24–31]. The lowest reported value for

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FIGURE 15. Scanning electron micrograph of GalnAsSb/AlGaAsSb laser structure.

 J_{th} is 1.5 kA/cm², which was obtained for lasers that used Al_xGa_{1-x}As_ySb_{1-y} layers with x = 0.55 [27]. Roomtemperature CW operation has been achieved by two groups [27, 28]. One of the groups, A.E. Bochkarev et al. [27], obtained threshold currents as low as 80 mA for ridge-waveguide lasers with an emission wavelength of 2.34 μ m.

Epitaxy of GaInAsSb/AlGaAsSb Laser Structure

Most of the previously reported GaInAsSb/AlGaAsSb lasers have been grown by liquid phase epitaxy (LPE). Although high-quality material can be grown by LPE, this technique has several limitations. First, there is a miscibility gap in the Ga_{1-x}In_xAs_ySb_{1-y} system for compositions with bandgaps that correspond to a wavelength region between 2.4 and 4 μ m [32]. Second, growth of lattice-matched AlGaAsSb layers becomes more difficult with increasing Al content because incorporation of sufficient As for lattice matching requires the growth temperature to be increased significantly [33]. Finally, because LPE does not provide good thickness control or uniformity, the technique is not well suited for fabricating quantum-well structures for higher-performance lasers.

Molecular-beam epitaxy (MBE), which does not have

such drawbacks, has also been used to grow GaInAsSb/ AlGaAsSb lasers [24, 31]. Before we started our research effort in late 1988, lasers grown by MBE had characteristics considerably inferior to lasers grown by LPE. The lowest threshold current density achieved at room temperature was 4.2 kA/cm² [24]. Our MBE-grown lasers have much improved characteristics, with J_{th} as low as 1.5 kA/cm² (equal to the lowest value reported [27] for GaInAsSb/AlGaAsSb devices), η_d as high as 50%, and pulsed output power as high as 1.8 W from both facets.

In MBE, epilayers are deposited on a heated substrate by the simultaneous evaporation of several beams of molecules in an ultrahigh vacuum [34]. The beam fluxes are individually controlled by adjusting the temperatures of the crucibles holding the different sources.

The sources we used for growing GaInAsSb and AlGaAsSb were the Group III and Group V elements, which yielded beams of Al, Ga, and In atoms, and As₄ and Sb₄ molecules. The n-type dopant was Te, which was provided by the sublimation of GaTe, and the ptype dopant was Be. As in the MBE growth of other III-V semiconductors, during epilayer deposition the total Group V flux was greater than the total Group III flux.

Lattice-matching the alloys to the substrate required

very careful adjustment of each beam flux. Because the total thickness of the AlGaAsSb cladding layers was ~5 μ m, the lattice mismatch $\Delta a la_{sub}$ would have to be less than 10⁻³ to avoid dislocation formation. (Note: $\Delta a = a_{epi} - a_{sub}$, where a_{epi} and a_{sub} are the lattice constants of the epilayer and substrate, respectively.) Because of its smaller thickness, the GaInAsSb active layer could tolerate a slightly larger lattice mismatch. Adjusting the fluxes of Al, Ga, and In was straightforward because their incorporation efficiency is equal to unity. Therefore, the ratio of these elements in an alloy epilayer is just equal to the ratio of their fluxes. Selecting the proper fluxes for Sb and As was more difficult, however, because Sb is incorporated much more readily than As. Consequently, we controlled the As and Sb mole fractions in GaInAsSb and AlGaAsSb by using a large excess As flux and reducing the ratio of Sb to the total Group III elements far enough below 1 to yield the desired composition.

The optimization of the growth conditions required a number of iterations. First, a test layer was characterized by X-ray diffraction to check the lattice mismatch, by Auger electron spectroscopy to examine the composition, and by infrared absorption to measure the approximate bandgap. Using this information, we adjusted the beam fluxes to obtain better lattice matching. When the lattice matching was acceptable, the layer was





further characterized by low-temperature photoluminescence to check the optical quality and to obtain a more precise bandgap measurement. We repeated these steps until satisfactory growth conditions were established.

The laser structures were grown on commercial Tedoped GaSb substrates. Figure 15 is a scanning electron micrograph that shows a cross section of a GaInAsSb/ AlGaAsSb laser structure. From bottom to top, the structure consists of a $0.2-\mu$ m-thick n⁺-GaSb buffer layer, a $2-\mu$ m-thick n-Al_{0.5}Ga_{0.5}As_{0.04}Sb_{0.96} cladding layer, a $0.4-\mu$ m-thick nominally undoped Ga_{0.84}In_{0.16}As_{0.14}Sb_{0.86} active layer, a $3-\mu$ m-thick p-Al_{0.5}Ga_{0.5}As_{0.04}Sb_{0.96} cladding layer, and an $0.05-\mu$ mthick p⁺-GaSb cap layer.

We selected the composition of the active layer for lasing at 2.3 μ m. The carrier concentrations in the nand p-AlGaAsSb cladding layers were about 1×10^{17} and 6×10^{16} cm⁻³, respectively. The doping concentration of the p⁺-GaSb cap layer was 2×10^{18} cm⁻³.

Figure 16 shows that the surface morphology of the laser structure was very smooth. Note, however, the cross-hatch pattern in the photomicrograph. The pattern is a result of a slight residual lattice mismatch. From a double-crystal X-ray diffraction measurement, we find the mismatch to be about 1.5×10^{-3} .

Laser Characteristics

We fabricated 300- μ m-wide broad-stripe lasers by a process similar to the one used to fabricate InGaAs/ AlGaAs lasers. The p⁺- and n-GaSb layers were metallized with Ti/Au and Au/Sn/Au, respectively, and the alloying was performed at 300°C in a H₂ atmosphere. (In a separate study of test samples, we measured specific contact resistances of less than 5 × 10⁻⁵ Ω -cm² for both the p and n contacts.) Next, the wafer was cleaved into bars with a cavity length *L* that ranged from 300 to 700 μ m. Using In, we then mounted the bars junction side up on copper heat sinks.

Figure 17 shows the current versus voltage characteristic of a 300×300 -µm GaInAsSb/AlGaAsSb laser. The turn-on voltage is about 0.25 V and the series resistance is about 1.5 Ω . In the reverse direction, the leakage current is about 250 and 500 µA at -1 and -2 V, respectively. The leakage current is sensitive to the amount of lattice mismatch and the quality of the epilayer material. In general, lasers with larger leakage currents have poorer lasing characteristics.

We probe-tested the lasers under pulsed condition at room temperature. Figure 18 shows the emission spectrum of a laser 300 μ m long at approximately 1.15 times the threshold current. The output shows multiple longitudinal modes, as is typically observed in broad-stripe lasers. The peak wavelength is located at 2.275 μ m, which is very close to the design wavelength of 2.3 μ m. From the mode spacing of about 23 Å, we find the group refractive index *n** to be about 3.71. The group refractive index is defined by

$$n^* \equiv n \left[1 - \frac{\lambda}{n} \left(\frac{dn}{d\lambda} \right) \right],$$

where *n* is the effective refractive index of the double heterostructure, and λ is the wavelength.



FIGURE 17. Voltage versus current for GalnAsSb/ AIGaAsSb laser.

Measuring the pulsed output power of the lasers is not a straightforward task because no large-area photodetector with high sensitivity and high speed is available for wavelengths beyond $2 \mu m$. We selected a pyroelectric detector because of its relatively low minimum detectable signal, wide dynamic range, and flat spectral response. Because of the low detector responsivity, however, the RF pickup noise was larger than the photosignal when the laser was placed close enough to the detector to avoid the use of collecting optics. Since the laser has a large beam divergence, we used an ellipsoidal reflector to collect most of the light. The laser was located at one focal point of the ellipse and the pyroelectric detector



FIGURE 18. Emission spectrum of GalnAsSb/AlGaAsSb diode laser for pulsed operation at room temperature.

was located at the other. We obtained the output power by dividing the average energy measured per pulse by the pulse width, which was generally 500 nsec.

Figure 19 shows the dependence of $J_{\rm th}$ on *L*. As *L* increases from 300 to 700 μ m, $J_{\rm th}$ decreases monotonically from 1.8 to 1.5 kA/cm², which is equal to the lowest reported value for GaInAsSb/AlGaAsSb lasers [27]. These values are considerably lower than the one calculated by A. Sugimura [35], who assumed that Auger recombination is the main nonradiative loss mechanism. In addition, $J_{\rm th}$ did not show any significant dependence on wavelength in the region from 1.8 to 2.3 μ m [26]. These results indicate that Auger recombination is not the dominant loss mechanism in this wavelength region.

Figure 20 is a plot of η_d^{-1} versus *L*. The value of η_d decreases from 47% for $L = 300 \ \mu m$ to 27% for



FIGURE 19. Dependence of threshold current density J_{th} on cavity length *L*.

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 $L = 700 \ \mu\text{m}$. From the slope of the straight line drawn through the data points and the assumption that R = 0.3, we calculate the internal loss coefficient α_i to be ~43 cm⁻¹, which is comparable to values obtained for InGaAsP/InP double-heterostructure lasers [36]. The internal quantum efficiency obtained from the *y*-intercept is ~100%.

Figure 21 shows the P-I characteristic of a 300×300 µm device. We reduced the pulse width to 200 nsec in order to decrease the temperature rise at the junction and to increase the current level that could be used without damaging the device at the point contact to the Ti/Au metallization. The value of η_d is ~50%, and the maximum power from both facets is 1.8 W, which was



FIGURE 20. Dependence of reciprocal differential quantum efficiency η_d^{-1} on cavity length *L*.

obtained at 9 A. (The output power was limited by the failure of the point contact.) These are the highest room-temperature values obtained for any semiconductor laser emitting beyond 2 μ m.

We measured P-I curves for another $300 \times 300 - \mu m$ laser at temperatures from -120 to 20° C. Figure 22, which plots J_{th} as a function of temperature, shows that $J_{th} = 190 \text{ A/cm}^2$ at -120° C. The characteristic temperature T_0 is ~75 K and 50 K near -120° C and 20° C, respectively. These values are comparable to the best values that have been reported for GaInAsSb/AlGaAsSb lasers [25, 27, 29]. The decrease of T_0 with increasing temperature may indicate that Auger recombination becomes more important at higher temperatures.

Figure 23 shows the near-field pattern recorded with a PbS camera for a 300×300 -µm device. Except for some filamentation that commonly exists in broad-stripe la-



FIGURE 21. Light output versus current for GalnAsSb/ AlGaAsSb laser 300 μ m wide by 300 μ m long. The data are for pulsed operation at 295 K.

sers, the pattern is fairly uniform, which indicates good spatial uniformity of the epilayers. The far-field pattern in the direction normal to the junction is shown in Figure 24. The FWHM is ~65°. The large divergence angle indicates a fairly tight confinement of the mode to the active layer, since this angle is inversely proportional to the beam size. The refractive index step, calculated by using an approximate expression relating this step to the divergence [37], is ~0.35. The refractive indexes of GaInAsSb and AlGaAsSb have not been measured.

Conclusion

Although relatively new, InGaAs/AlGaAs strained-layer quantum-well lasers have already demonstrated state-ofthe-art performance. Their rapid progress has been possible because the technology that has been developed for the growth and fabrication of GaAs/AlGaAs lasers is directly applicable. With the benefit of enhanced reli-



FIGURE 22. Dependence of threshold current density J_{th} on temperature for GalnAsSb/AlGaAsSb laser 300 μ m wide \times 300 μ m long.



FIGURE 23. Near-field pattern of GalnAsSb/AlGaAsSb laser measured by PbS camera.

ability that results from the addition of In, InGaAs/ AlGaAs lasers will be extremely useful for applications requiring emission wavelengths in the range from 0.9 to $1.1 \,\mu$ m.

While GaInAsSb/AlGaAsSb lasers are still in an early stage of development, the results already obtained are much better than had been anticipated. With many applications awaiting lasers that emit at 2 to 4 μ m, the field is wide open for much work. Areas that call for further effort include optimization of the epilayer growth parameters, development of index-guided structures for low threshold currents, development of quantum-well



FIGURE 24. Far-field pattern of GalnAsSb/AlGaAsSb laser in the direction normal to the junction.

structures for improved performance, and extension of the emission wavelength to 4 μ m, as well as additional theoretical study of the material system and measurement of basic parameters such as the refractive index.

Acknowledgments

The authors are grateful for the expert technical assistance of M.K. Connors, B. DiGiorgio, W.L. McGilvary, and G.D. Silva in laser fabrication; and of D.F. Kolesar and B.A. Nechay in establishing the laser-measurement setup. The authors also acknowledge the contributions of G.W. Turner and J.W. Chludzinski for photoluminescence and laser emission spectroscopy; P.M. Nitishin for scanning electron microscopy; and J.V. Pantano and D.M. Tracy for epitaxial growth. The continued interest and helpful suggestions of A.J. Strauss and I. Melngailis are gratefully appreciated.

This work was sponsored by the Department of the Air Force.

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